

LA--1061

CIC-14 REPORT COLLECTION  
REPRODUCTION  
COPY

~~Copy 14~~ Of 28

Series..A

c.3

# LOS ALAMOS SCIENTIFIC LABORATORY

OF THE

UNIVERSITY OF CALIFORNIA

CONTRACT W-7405-ENG. 36 WITH

U. S. ATOMIC ENERGY COMMISSION



CLASSIFICATION CANCELLED  
For The Atomic Energy Commission  
by the Declassification Officer  
per Dec. 20, 1977  
5-8-80  
V. R.

LA - 1061

Series A

This is copy 14 of 28 copies

January 24, 1950

This document contains 10 pages

NEUTRON DIFFUSION THEORY THE TRANSPORT APPROXIMATION

Work Done By:

Bengt Carlson  
Marian Peterson

Written By:

Bengt Carlson



General Physics



## NEUTRON DIFFUSION THEORY\*

### THE TRANSPORT APPROXIMATION

One-velocity neutron diffusion problems involving anisotropic scattering are considerably simplified if one applies the so-called Transport Approximation. The latter consists in replacing, in the formulae for isotropic scattering, the scattering cross section  $\sigma_s$  wherever it occurs by the corresponding transport cross section  $\bar{\sigma}_s$  to be defined below.

The accuracy of the Transport Approximation has not been thoroughly investigated. In this Report it will be checked against exact theory in the simple problem of calculating the critical radius of a bare sphere in the case of linear anisotropy. The comparison of approximate and exact theory in this special case will give an indication of the error to be expected in similar problems, but good agreement in this case does not of course justify the Transport Approximation in general.

#### Notation

We consider the processes of scattering, absorption, and fission and denote the corresponding cross sections by  $\sigma_s$ ,  $\sigma_a$ , and  $\sigma_f$ , letting  $\sigma_t = \sigma_s + \sigma_a + \sigma_f$ ,  $\nu$  = the number of neutrons emerging per fission and  $N$  the number of nuclei per  $\text{cm}^3$ . We assume that the fission neutrons are ejected isotropically, and that the scattered neutrons emerge according to the scattering law:

---

\* This Report is based on a set of notes by G. Placzek.

$$(1) \quad F(\mu) = \frac{1}{2} [1 + 3b_1 P_1(\mu) + 5b_2 P_2(\mu) + \dots]$$

where  $\mu = \cos \theta$ , and  $\theta$  the angle of deflection. In this Report, we restrict the discussion to linear scattering, in which case (1) reduces to:

$$(2) \quad F(\mu) = \frac{1}{2} (1 + 3b_1 \mu)$$

where  $|b_1| \leq \frac{1}{3}$ . We shall refer to  $b_1$  as the "transport" and define  $\bar{\sigma}_S$  as follows:

$$(3) \quad \bar{\sigma}_S = \sigma_S (1 - b_1).$$

For the isotropic case we have  $b_1 = 0$  and  $\bar{\sigma}_S = \sigma_S$ . From (2) we also have:

$$(4) \quad \int_{-1}^1 F(\mu) d\mu = 1, \quad \int_{-1}^1 F(\mu) \mu d\mu = b_1.$$

### Exact Theory

In the exact theory, we work with the following parameters:

$$(5) \quad \begin{cases} \sigma = \sigma_f N \\ c \equiv 1 + f = \frac{\sigma_S + 2\sigma_f}{\sigma_f} \\ b \equiv \frac{\alpha}{3c} = \frac{1}{c} \cdot \frac{\sigma_f}{\sigma_f} \cdot b_1 \end{cases}$$

where  $b$  is the effective transport obtained by combining isotropic fission with anisotropic scattering. In addition, the parameter  $k$ , a function of  $c$  and  $b$ , is obtained from the equation:

$$(6) \quad c \frac{\arctan k}{k} - \frac{(c-1)\alpha}{k^2} \left( 1 - \frac{\arctan k}{k} \right) = 1.$$

Three general methods are available for the calculation of the critical radius  $\sigma a$  of a bare sphere. The accuracy of these methods has been investigated in a number of LA Reports. The error in the Endpoint Method<sup>1)</sup> increases from 0 to about 0.2 % as  $C$  goes from 1 to 3, and for  $C = \infty$  the error is 2.1 %. The error in the Serber-Wilson Method<sup>2)</sup> increases rapidly from 0 to about 4 % as  $C$  goes from 1 to 1.2. The error then stays nearly constant at about 4 % in the  $C$ -interval  $(1.2, \infty)$ . The error in the Iterative Method<sup>3)</sup> with a quadratic trial function decreases from about 0.2 % to 0 % as  $C$  goes from 1.2 to  $\infty$ . For  $C$ -values very close to 1, the method breaks down.

#### The Endpoint Method

Using this method we have:

$$(7) \quad \sigma a = \frac{\pi}{k} - z_0.$$

The quantity  $k = k(c, b)$  is obtained from equation (6), and  $z_0 = z_0(c, b)$  for  $b=0$  from LAMS-806:

$$(8) \quad CZ_0(c, 0) \equiv (1+f_1)Z_0(1+f_1, 0) = 1 - (1+f_1)AX(f_1, f_2), \text{ with } f_2 = -1.$$

where the notation of LAMS-806 is used on the right hand side.

For  $b \neq 0$ , the formula for  $Z_0$  is given in B. Davison: Memorandum IV,<sup>4)</sup> Formula (3.23), but computation using this was not attempted because of the considerable labor involved.

#### The Serber-Wilson Method

Using this method,  $\sigma a$  is obtained as the solution of the equation:

$$(9) \quad \text{Im } E_1(\sigma a(1+ki)) = -e^{-\sigma a} \frac{\alpha \frac{f}{k}}{(1+f) + \alpha \frac{f}{k}} \frac{\sin k \sigma a}{k \sigma a}$$

where the function  $\text{Im } E_1(x+iy)$  is tabulated in AM-509.

This method has not been used since it is not accurate enough for the purpose of this Report.

### The Iterative Method

This method gives  $\sigma_a$  as the solution of the following matrix equation, where  $X$  denotes  $\sigma_a$ :

$$(10) \quad \begin{vmatrix} \frac{1}{3} \left[ \frac{1}{\bar{c}} - (P_{00}(x) + \frac{\alpha}{3} \frac{c-1}{c} Q_{00}(x)) \right], & \frac{1}{5} \left[ \frac{1}{\bar{c}} - (P_{02}(x) + \frac{\alpha}{5} \frac{c-1}{c} Q_{02}(x)) \right] \\ \frac{1}{5} \left[ \frac{1}{\bar{c}} - (P_{20}(x) + \frac{\alpha}{5} \frac{c-1}{c} Q_{20}(x)) \right], & \frac{1}{7} \left[ \frac{1}{\bar{c}} - (P_{22}(x) + \frac{\alpha}{7} \frac{c-1}{c} Q_{22}(x)) \right] \end{vmatrix} = 0$$

where the functions  $P_{ij}$  and  $Q_{ij}$  are defined and tabulated in LA-990.

### Transport Approximation

In the Transport Approximation, we work with the following parameters:

$$(11) \quad \begin{cases} \bar{\sigma} = \sigma_0 (1 - \frac{\alpha}{3}) N \\ \bar{c} \equiv 1 + \bar{f} = \frac{c - \frac{\alpha}{3}}{1 - \frac{\alpha}{3}} = 1 + \frac{c-1}{1 - \frac{\alpha}{3}} \\ \bar{b} = 0 \end{cases}$$

where  $\alpha$ ,  $|\alpha| \leq 1$ , is defined in (5).

### The Endpoint Method

$$(12) \quad \sigma_a = \frac{1}{1 - \frac{\alpha}{3}} \left[ \frac{\pi}{k(\bar{c})} - z_0(\bar{c}) \right].$$

### The Serber-Wilson Method

$$(13) \quad \text{Im } E_1 \left[ \left(1 - \frac{\alpha}{3}\right) \sigma_a (1 + ki) \right] = 0, \quad k = k(\bar{c}).$$

The Iterative Method

$$(14) \quad \left| \begin{array}{cc} \frac{1}{3} \left[ \frac{1}{c} - P_{00}(\sigma a) \right], & \frac{1}{3} \left[ \frac{1}{c} - P_{02}(\sigma a) \right] \\ \frac{1}{5} \left[ \frac{1}{c} - P_{20}(\sigma a) \right], & \frac{1}{7} \left[ \frac{1}{c} - P_{22}(\sigma a) \right] \end{array} \right| = 0.$$

Expansions for  $c$  Close to Unity.Exact Theory:

$$(15) \quad \frac{\sigma a_c}{\sigma a_{c=0}} = \frac{1}{\sqrt{1-b}} \left\{ 1 - .3917 \left( \frac{1}{\sqrt{1-b}} - 1 \right) \sqrt{c-1} + \left[ \frac{b}{2(1-b)} - .1534 \left( \frac{1}{\sqrt{1-b}} - 1 \right) \right] (c-1) + \dots \right\}.$$

Transport Approximation:

$$(16) \quad \frac{\sigma a_c}{\sigma a_{c=0}} = \frac{1}{\sqrt{1-b}} \left\{ 1 - .3917 \left( \frac{1}{\sqrt{1-b}} - 1 \right) \sqrt{c-1} + \left[ \frac{b}{10(1-b)} - .1534 \left( \frac{1}{\sqrt{1-b}} - 1 \right) \right] (c-1) + \dots \right\}.$$

Results

The results of the computations are presented in a graph at the end of this Report and in the following tables:

Table Ia	Transport Approximation, $\sigma a$ by the Endpoint Method.
Table Ib	Transport Approximation, $\sigma a$ by the Iterative Method.
Table IIa	Transport Approx., $\left( \frac{1+b}{2} \right) \left[ \frac{\sigma a_c}{\sigma a_{c=0}} - 1 \right]$ by the Endpoint Method.
Table IIb	Transport Approx., $\left( \frac{1+b}{2} \right) \left[ \frac{\sigma a_c}{\sigma a_{c=0}} - 1 \right]$ by the Iterative Method.
Table III	Exact Theory, $\sigma a$ and $\left( \frac{1+b}{2} \right) \left[ \frac{\sigma a_c}{\sigma a_{c=0}} - 1 \right]$ by the Iterative Method.

Table IaTransport Approximation,  $\sigma_a$  by the Endpoint Method

$f \backslash \alpha$	-1.0	-0.5	0.0	0.5	1.0
.00	$\infty$	$\infty$	$\infty$	$\infty$	$\infty$
.05	6.408	6.800	7.277	7.875	8.657
.1	4.329	4.576	4.873	5.240	5.709
.2	2.855	3.000	3.172	3.379	3.637
.4	1.8186	1.8961	1.9853	2.0896	2.2139
.6	1.3686	1.4190	1.4759	1.5410	1.6165
.8	1.1069	1.1429	1.1830	1.2280	1.2790
1.0	0.9331	0.9603	0.9901	1.0232	1.0602
1.2	0.8082	0.8295	0.8527	0.8781	0.9061
1.4	.7137	.7309	.7494	.7695	.7914
1.6	.6395	.6536	.6688	.6851	.7027
1.8	.5796	.5914	.6041	.6175	.6320
2.0	.5301	.5402	.5509	.5622	.5742
$\infty$	.0000	.0000	.0000	.0000	.0000

Table IbTransport Approximation,  $\sigma_a$  by the Iterative Method

$f \backslash \alpha$	-1.0	-0.5	0.0	0.5	1.0
.00	-	-	-	-	-
.05	-	-	-	-	-
.1	4.353	4.600	4.895	5.258	5.725
.2	2.862	3.007	3.178	3.385	3.642
.4	1.8209	1.8981	1.9871	2.0910	2.2154
.6	1.3696	1.4200	1.4769	1.5420	1.6176
.8	1.1077	1.1436	1.1838	1.2290	1.2803
1.0	0.9336	0.9608	0.9909	1.0242	1.0617
1.2	0.8088	0.8302	0.8535	0.8792	0.9078
1.4	.7143	.7316	.7503	.7707	.7934
1.6	.6401	.6544	.6697	.6864	.7047
1.8	.5802	.5923	.6050	.6190	.6340
2.0	.5308	.5412	.5520	.5638	.5764
$\infty$	.0000	.0000	.0000	.0000	.0000



Table IIa

Transport Approximation,  $(\frac{1}{2}) \frac{f(\alpha)}{f(0)} - 1$  by the Endpoint Method

$f \backslash \alpha$	-1.0	-0.5	0.5	1.0
.00	-.1340	-.0742	0.0954	0.2247
.05	-.1254	-.0688	.0863	.1991
.1	-.1228	-.0670	.0828	.1887
.2	-.1199	-.0651	.0783	.1759
.4	-.1176	-.0629	.0736	.1612
.6	-.1163	-.0617	.0706	.1524
.8	-.1158	-.0610	.0685	.1461
1.0	-.1151	-.0602	.0669	.1416
1.2	-.1148	-.0599	.0655	.1378
1.4	-.1143	-.0592	.0644	.1345
1.6	-.1139	-.0591	.0634	.1318
1.8	-.1136	-.0589	.0621	.1293
2.0	-.1133	-.0583	.0615	.1269
$\infty$	-.1172	-.0586	.0586	.1172

Table IIb

Transport Approximation,  $(\frac{1}{2}) \frac{f(\alpha)}{f(0)} - 1$  by the Iterative Method

$f \backslash \alpha$	-1.0	-0.5	0.5	1.0
.00	-	-	-	-
.05	-	-	-	-
.1	-.1218	-.0663	0.0816	0.1865
.2	-.1193	-.0646	.0782	.1752
.4	-.1171	-.0627	.0732	.1608
.6	-.1162	-.0616	.0705	.1524
.8	-.1157	-.0611	.0687	.1467
1.0	-.1157	-.0608	.0672	.1429
1.2	-.1152	-.0601	.0662	.1400
1.4	-.1152	-.0598	.0653	.1379
1.6	-.1149	-.0594	.0648	.1359
1.8	-.1148	-.0588	.0648	.1342
2.0	-.1152	-.0587	.0641	.1326
$\infty$	-.1165	-.0582	.0582	.1165

Table III

Exact Theory,  $\sigma_a$  by the Iterative Method

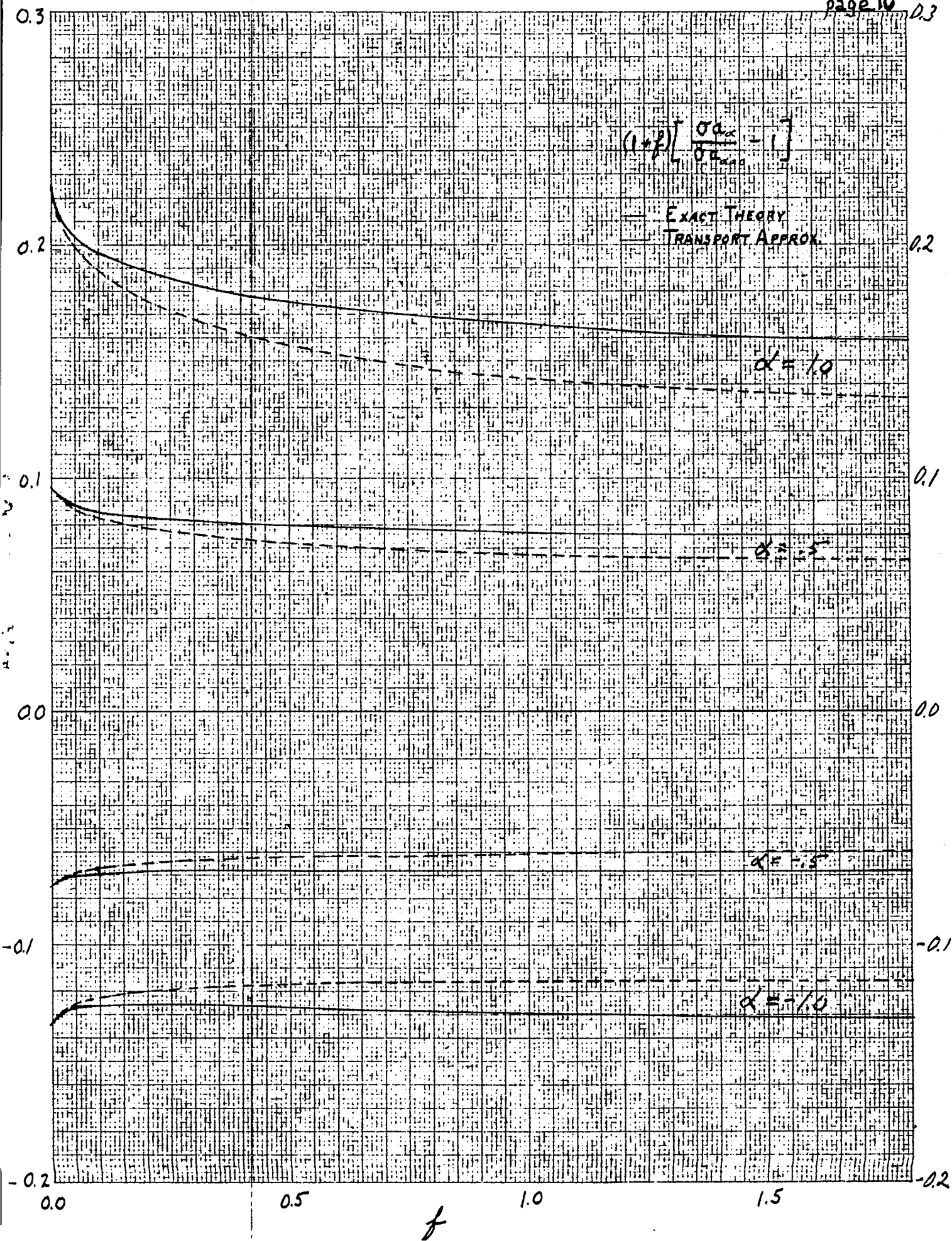
$f \backslash \alpha$	-1.0	-0.5	0.0	0.5	1.0
.00	—	—	—	—	—
.05	—	—	—	—	—
.1	4.333	4.585	4.895	5.276	5.770
.2	2.846	2.997	3.178	3.396	3.678
.4	1.8081	1.8907	1.9871	2.1015	2.2408
.6	1.3593	1.4140	1.4769	1.5498	1.6364
.8	1.0993	1.1388	1.1838	1.2350	1.2946
1.0	0.9269	0.9570	0.9909	1.0290	1.0728
1.2	.8031	.8270	.8535	0.8831	0.9167
1.4	.7094	.7289	.7503	.7740	.8005
1.6	.6359	.6521	.6697	.6892	.7108
1.8	.5766	.5902	.6050	.6212	.6393
2.0	.5276	.5394	.5520	.5656	.5808
$\infty$	.0000	.0000	.0000	.0000	.0000

Exact Theory,  $(1+f) \left[ \frac{\sigma_a}{\sigma_a - 1} \right]_{\alpha=0}$  by the Iterative Method

$f \backslash \alpha$	-1.0	-0.5	0.5	1.0
.00	—	—	—	—
.05	—	—	—	—
.1	-.1263	-.0697	0.0856	0.1966
.2	-.1254	-.0683	.0823	.1888
.4	-.1261	-.0679	.0806	.1787
.6	-.1274	-.0681	.0790	.1728
.8	-.1285	-.0684	.0779	.1685
1.0	-.1292	-.0684	.0769	.1653
1.2	-.1299	-.0683	.0763	.1629
1.4	-.1308	-.0685	.0758	.1606
1.6	-.1312	-.0683	.0757	.1596
1.8	-.1314	-.0685	.0750	.1587
2.0	-.1326	-.0685	.0739	.1565
$\infty$	-.1410	-.0705	.0705	.1410

$$(1+f) \left[ \frac{\sigma_{ax}}{\sigma_{ax_0}} - 1 \right]$$

— EXACT THEORY  
— TRANSPORT APPROX.



DOCUMENT ROOM

REC. FROM Eng-1

DATE 2-1-50

REC. NO. REC.